


# Basic Electrical Engineering

## KEE101/201

Department of Engineering  
Uttar Pradesh Textile Technology Institute  
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Semester-II  
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# Ideal Vs Practical Transformer



- Coil resistance is zero (Lossless)
- Core material has infinite permeability
- No flux Leakages (All flux is linked with the core)
- No eddy current losses, No Hysteresis Losses.
- Coil resistance is present though it is low.
- Core material has finite permeability
- Some Flux Leakages occur through air. Represented by Leakage reactance.
- Eddy current and Hysteresis Losses are present. (core or Fixed Losses)

# Ideal Transformer on Load



- $V_1 = \text{Applied ac Voltage (RMS)}$
- $E_1 = 4.44f\phi_m N_1$
- $E_2 = 4.44f\phi_m N_2$
- $E_1 = \text{Induced Voltage in Primary (RMS)}$
- $E_2 = \text{Induced Voltage in Secondary (RMS)}$
- $V_2 = \text{Terminal ac secondary Voltage (RMS)}$
- $\frac{E_1}{E_2} = \frac{N_1}{N_2} = \frac{V_1}{V_2}$

# Ideal Transformer on Load



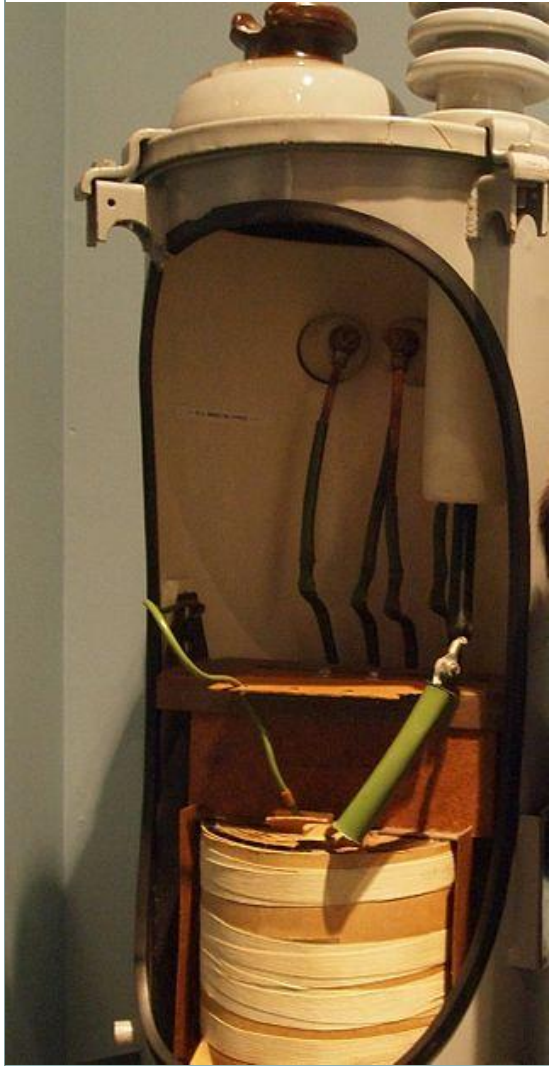
- *Excitation current is zero for primary  $N_1$*
- *$I_2 =$  Secondary current when load is connected*
- *$N_2 I_2 =$  Secondary mmf*
- *$N_1 I_1 =$  Primary counter mmf*
- *$N_2 I_2 = N_1 I_1$*
- $$\frac{N_1}{N_2} = \frac{I_2}{I_1}$$

# Ideal Vs Practical Transformer



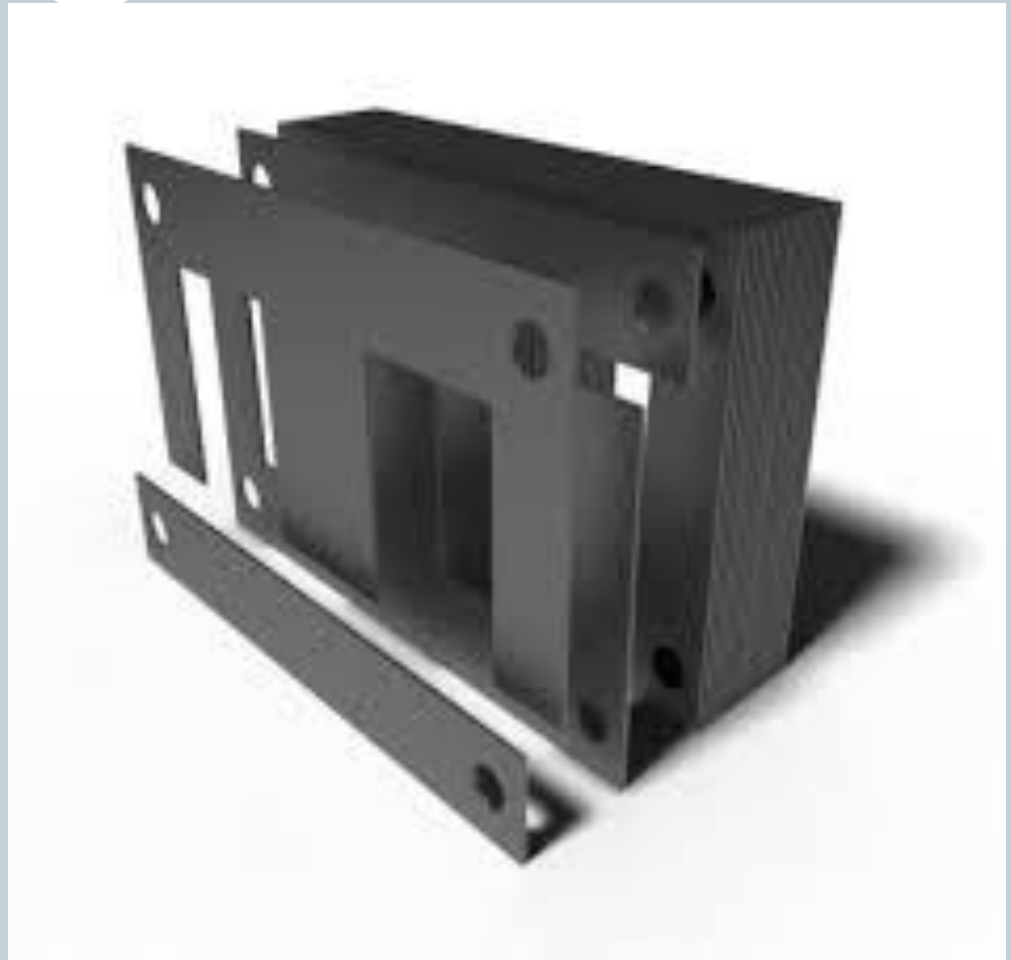
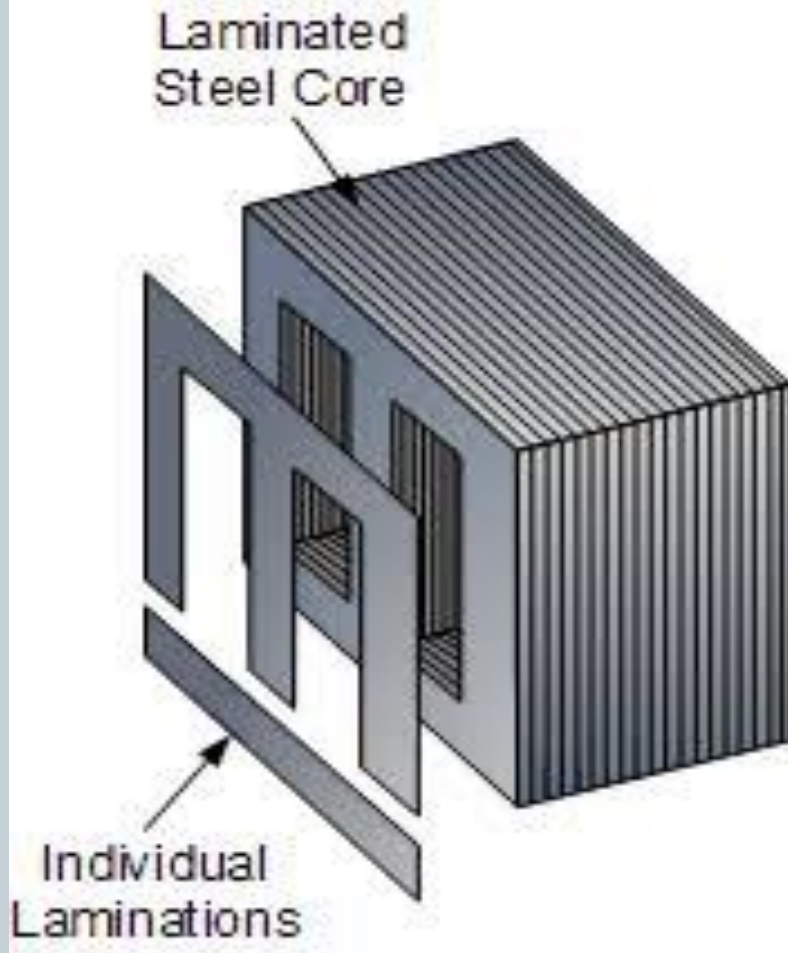
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# Practical 1-Phase Transformer: Construction

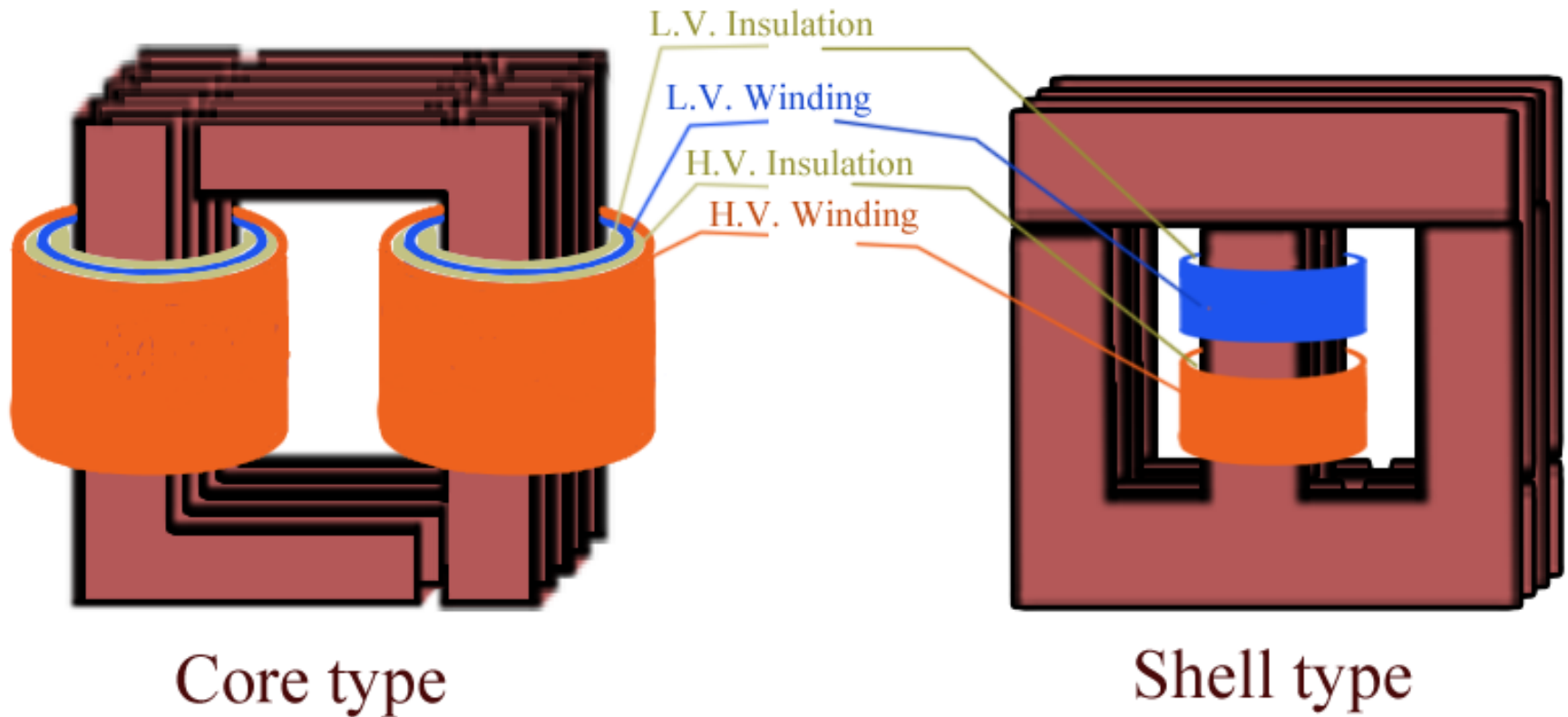




# Transformer: Construction



# Transformer: Construction





# Transformer: Important Parts

- Core

- Core Type
- Shell Type

- Winding

- LV (Low Voltage) Winding
- HV (High Voltage) Winding

- Insulation

- Major Insulation
- Minor Insulation

- Protection

Windings on side limbs  
Enclose the core

Core Encloses the Windings on Central Limb

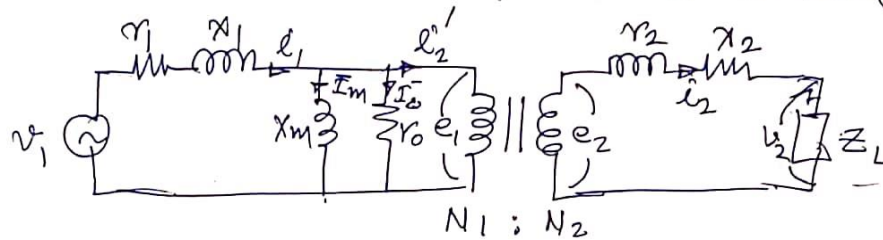
Thick Wire More current to carry

Thin Wire, Less Current

Between Windings and Container

Between winding turns and Layers

# Ideal Transformer Vs Practical



$X_m$  = magnetizing reactance to account for  $\bar{I}_m$  (in) - the magnetizing current when some finite reluctance will be there i.e. core of a practical transformer

$r_0$  = Core loss resistor to account for the losses i.e. eddy current and hysteresis loss. (current  $\bar{I}_0$  is there).

$$\bar{I}_m + \bar{I}_0 = \bar{I}_e$$

$$\bar{V}_1 = r_1 \bar{I}_1 + jX_1 \bar{I}_1 + \bar{E}_1$$

$$\bar{E}_2 = r_2 \bar{I}_2 + jX_2 \bar{I}_2 + \bar{V}_2$$

$$\bar{V}_2 = \bar{I}_2 Z_L$$

$$\bar{I}_1 = \bar{I}_2' + \bar{I}_e$$

$$\bar{I}_m = \frac{E_1}{jX_m}$$

$$\bar{I}_0 = \frac{E_1}{r_0}$$

$$\bar{I}_2' = \frac{N_2}{N_1} \bar{I}_2$$

## Relaxing Assumptions of Ideal Transformer

## And Introducing

Coil Resistances

Leakage Reactance

Magnetizing Reactance

Core Loss Resistance

Magnetizing Current

Core loss Current

Primary Current

Secondary Current

Secondary Reflection current

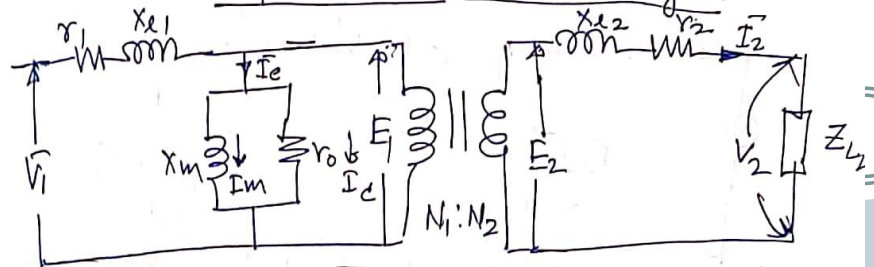
Transformer Equations

Exact Equivalent Circuit

# Introducing

- The Following Quantities referred to primary
- Secondary Leakage Reactance
- Secondary Resistance
- Secondary Load Impedance
- Transformer Equations
- Exact Equivalent Circuit

Equivalent Circuit Diagram



Equation 1:  $\bar{V}_1 = r_1 \bar{I}_1 + j X_{l1} \bar{I}_1 + \bar{E}_1$

Equation 2:  $\bar{E}_2 = r_2 \bar{I}_2 + j X_{l2} \bar{I}_2 + \bar{V}_2$

Equation 3:  $\bar{V}_2 = \bar{I}_2 Z_L$

$\bar{E}_2 = (r_2 + j X_{l2}) \bar{I}_2 + \bar{V}_2 = (r_2 + j X_{l2} + Z_L) \bar{I}_2$

$\bar{I}_2' = \frac{N_2}{N_1} \bar{I}_2$

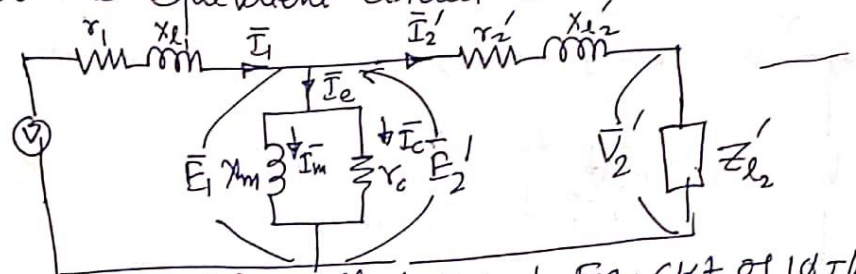
$\bar{I}_2' = \frac{N_2}{N_1} \frac{E_2}{(r_2 + j X_{l2} + Z_L)}$   
 $= \left(\frac{N_2}{N_1}\right)^2 \frac{\left(\frac{N_1}{N_2} E_2\right)}{(r_2 + j X_{l2} + Z_L)} \rightarrow \bar{E}_1$

$\bar{I}_2' = \frac{\bar{E}_1}{\left(\frac{N_1}{N_2}\right)^2 \{ r_2 + j X_{l2} + Z_L \}}$

if this resist impedance is multiplied by  $\left(\frac{N_1}{N_2}\right)^2$  the combined impedance may be seen to be connected across  $\bar{E}_1$ , replacing ideal transformer and the secondary circuit.

Referred Impedances.

So the equivalent circuit becomes:-



This circuit is called Exact Eq. Ckt of 1ϕ TR

Where  $r_2' = \left(\frac{N_1}{N_2}\right)^2 r_2$   
 $x_{L2}' = \left(\frac{N_1}{N_2}\right)^2 x_{L2}$   
 $Z_{L2}' = \left(\frac{N_1}{N_2}\right)^2 Z_{L2}$

These quantities are called secondary impedances referred to primary.

if we check power consumption in secondary resistance:

In actual circuit it is =  $I_2^2 r_2$

In exact eq. ckt it is =  $(I_2')^2 \cdot r_2'$   
 $= \left(\frac{N_2}{N_1} I_2\right)^2 \cdot \left(\frac{N_1}{N_2}\right)^2 \cdot r_2$   
 $= \frac{N_2^2}{N_1^2} I_2^2 \cdot \frac{N_1^2}{N_2^2} \cdot r_2$   
 $= I_2^2 r_2$

which is same as in actual ckt.

Referred voltages

Power in referred ckt (kVA this time)

$$\bar{V}_2 = \bar{I}_2 Z_{l2} \quad \text{actual ckt}$$

$$\bar{V}_2' = \bar{I}_2' \cdot Z_{l2}' \quad \text{referred ckt}$$

$$\bar{V}_2' = \left( \frac{N_2}{N_1} I_2 \right) \left( \frac{N_1}{N_2} \right)^2 Z_{l2}$$

$$= \left( \frac{N_1}{N_2} \right) I_2 Z_{l2} = \frac{N_1}{N_2} \cdot \bar{V}_2$$

$$\boxed{\bar{V}_2' = \frac{N_1}{N_2} \bar{V}_2} \quad \text{and} \quad \boxed{\bar{I}_2' = \frac{N_2}{N_1} \bar{I}_2}$$

Total Power in referred ckt.

$$\bar{P}_2' = \bar{V}_2' \bar{I}_2' = \frac{N_1}{N_2} \bar{V}_2 \cdot \frac{N_2}{N_1} \bar{I}_2 \quad (\text{kVA})$$

$$= \bar{V}_2 \bar{I}_2 = \text{Power in actual ckt} \quad (\text{kVA})$$